



Storage Allocation and **Investment** Optimization for **Transmission Constrained Networks Considering Losses** and High Renewable Penetration

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# Context and Motivation



#### Context



#### Renewable Energy Sources (RES)

- Increase of RES share in the following years
- Intermittency issues and no output control

#### Energy Storage Systems (ESS)

- Promising option to soften renewable intermittency and increase flexibility
- New developments are reducing the costs, especially for electrical ESS



#### **Motivation**



Wide number of ESS technologies and characteristics
Different energy/power ratios
Multiple services: time shifting, ramping etc.

# Real Power System characteristics

- Network Congestion
- Transmission Losses



#### **Research Questions**



• What is the impact of network congestion or transmission losses on ESS allocation/ investment decisions?

 How does the level of renewable penetration in a power system change the ESS investment decisions?





# Optimization Model and Metrics

# Optimization Model General Description

#### **Objective Function:**

Minimize production costs

#### Subject to:

- Power balance constraint
- Storage balance constraint
- Charge/discharge limits
- Storage limits
- Final storage level condition
- Thermal units limits
- Ramp limits for thermal units
- Maximum Storage to be installed
- Transmission network constraints (DC-OPF)
- Piecewise Linear Approximation for transmission losses





| Metric                                      | Purpose  | Equation  |
|---|--|---|
| Overall<br>Capacity<br>Metric (OM)          | To compare the maximum storage<br>level in MWh attained over the time<br>horizon to the actual amount of<br>capacity of that technology installed<br>at each node      | $OM_{jn} = 1 - \frac{max_t\{s_{jn}(t)\}}{k_{jn}}$                                   |
| Cycling<br>Metric (CM)                      | To keep tracking of how many full<br>charging cycles a technology goes<br>through over the total time horizon<br>at each node  | $CM_{jn} = \frac{\sum_{t \in T} \left[ r_{jn}^c(t) \cdot \Delta t \right]}{k_{jn}}$ |
| Overall<br>Storage<br>Level Metric<br>(OSL) | To provide an idea of how much<br>energy each technology stores<br>throughout a day for each scenario in<br>comparison to the base case of an<br>unconstrained network | $OSL_{j} = \frac{\sum_{n,t} s_{jn}(t)}{\sum_{n,t} s\_BaseCase_{jn}(t)}$             |



## Case Study







#### Modified IEEE 14 Bus System



Data information from:

S. Wogrin y D. F. Gayme, «Optimizing Storage Siting, Sizing, and Technology Portfolios in Transmission-Constrained Networks», IEEE Trans. Power Syst., vol. 30, n.o 6, pp. 3304-3313, nov. 2015.

Storage Allocation Results







### Impact of Transmission Losses

The introduction of losses into the model led to changes in the *spatial distribution of storage capacity* and the temporal usage of each technology



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### Impact of Transmission Congestion

#### **No Congestion**

#### Congestion



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#### Results obtained for the Metrics

| Cara Studie  | Tash  | C       | М       | 0      | М      | OSL   |
|--|-------|---------|---------|--------|--------|-------|
| Case Study   | 1 ech | n3      | n9      | n3     | n9     |       |
|  | PSH   | 0.0025  | 0.0025  | 0.9999 | 0.9999 | 1.00  |
| Congestion = NO  | CAES  | 0.0031  | 0.0031  | 1.0000 | 1.0000 | 0.00  |
| Losses = NO  | LION  | 1 7335  | 1 7335  | 0.9286 | 0.9286 | 1.00  |
|  | FES   | 5.3050  | 5.3050  | 0.9286 | 0.9286 | 1.00  |
| and the second sec | PSH   | 0.0037  | 0.0011  | 0.9998 | 0.9999 | 1.24  |
| Congestion = NO  | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| Losses = YES   | LION  | 3.1188  | 1.0445  | 0.8863 | 0.9799 | 1.00  |
|  | FES   | 18.0912 | 10.6613 | 0.7088 | 0.8669 | 1.00  |
|  | PSH   | 0.1265  | 0.0000  | 0.9918 | 1.0000 | 15.53 |
| Congestion =   | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| YES  | LION  | 1 1742  | 2.1102  | 0.0937 | 1.0000 | 1.07  |
| Losses = NO  | FES   | 6.6397  | 0.0000  | 0.2446 | 1.0000 | 1.11  |
|  | PSH   | 0.0898  | 0.0000  | 0.9923 | 1.0000 | 15.80 |
| Congestion =   | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| I ES   | LION  | 1 0396  | 0.0000  | 0.1081 | 1.0000 | 1.07  |
| Losses = YES   | FES   | 6.1778  | 0.0000  | 0.2582 | 1.0000 | 1.09  |

The CM indicates that FES goes through the most full cycles of any technology in the portfolio. This is likely attributed to its short ramp time which allows it to fully charge and discharge within a single timestep.

When losses are introduced, the number of cycles more than triples at node 3 and doubles at node 9 even though the overall capacity remains unchanged.

#### **Results obtained for the Metrics**

| Care Stude      | Tash  | C       | М       | 0      | OSL    |       |  |
|-----------------|-------|---------|---------|--------|--------|-------|--|
| Case Study      | 1 ech | n3      | n9      | n3     | n9     |       |  |
|                 | PSH   | 0.0025  | 0.0025  | 0.9999 | 0.9999 | 1.00  |  |
| Congestion = NO | CAES  | 0.0031  | 0.0031  | 1.0000 | 1.0000 | 0.00  |  |
| Losses = NO     | LION  | 1.7335  | 1.7335  | 0.9286 | 0.9286 | 1.00  |  |
|                 | FES   | 5.3050  | 5.3050  | 0.9286 | 0.9286 | 1.00  |  |
| and the second  | PSH   | 0.0037  | 0.0011  | 0.9998 | 0.9999 | 1.24  |  |
| Congestion = NO | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |  |
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|                 | FES   | 18.0912 | 10.6613 | 0.7088 | 0.8669 | 1.00  |  |
|                 | PSH   | 0.1265  | 0.0000  | 0.9918 | 1.0000 | 15.53 |  |
| Congestion =    | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |  |
| YES             | LION  | 1.1742  | 2.1102  | 0.0937 | 1.0000 | 1.07  |  |
| Losses = NO     | FES   | 6.6397  | 0.0000  | 0.2446 | 1.0000 | 1.11  |  |
|                 | PSH   | 0.0898  | 0.0000  | 0.9923 | 1.0000 | 15.80 |  |
| Congestion =    | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |  |
| I ES            | LION  | 1.0396  | 0.0000  | 0.1081 | 1.0000 | 1.07  |  |
| Losses = YES    | FES   | 6.1778  | 0.0000  | 0.2582 | 1.0000 | 1.09  |  |

The OM indicates that in a non-congested network, the capacity allocated in node 3 is almost fully used for all the technologies. However, when the network is congested, the allocation of FES capacity is not used due to the transmission constraints, and OM metrics shows how almost 75% of this capacity is unused.

#### **Results obtained for the Metrics**

| Corres Stracker | Tal   | C       | М       | 0      | М      | OSL   |
|-----------------|-------|---------|---------|--------|--------|-------|
| Case Study      | 1 ecn | n3      | n9      | n3     | n9     |       |
|                 | PSH   | 0.0025  | 0.0025  | 0.9999 | 0.9999 | 1.00  |
| Congestion = NO | CAES  | 0.0031  | 0.0031  | 1.0000 | 1.0000 | 0.00  |
| Losses = NO     | LION  | 1.7335  | 1.7335  | 0.9286 | 0.9286 | 1.00  |
|                 | FES   | 5.3050  | 5.3050  | 0.9286 | 0.9286 | 1.00  |
|                 | PSH   | 0.0037  | 0.0011  | 0.9998 | 0.9999 | 1.24  |
| Congestion = NO | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| Losses = YES    | LION  | 3.1188  | 1.0445  | 0.8863 | 0.9799 | 1.00  |
|                 | FES   | 18.0912 | 10.6613 | 0.7088 | 0.8669 | 1.00  |
|                 | PSH   | 0.1265  | 0.0000  | 0.9918 | 1.0000 | 15.53 |
| Congestion =    | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| YES             | LION  | 1.1742  | 2.1102  | 0.0937 | 1.0000 | 1.07  |
| Losses = NO     | FES   | 6.6397  | 0.0000  | 0.2446 | 1.0000 | 1.11  |
| C               | PSH   | 0.0898  | 0.0000  | 0.9923 | 1.0000 | 15.80 |
| Congestion =    | CAES  | 0.0000  | 0.0000  | 1.0000 | 1.0000 | 0.00  |
| I ES            | LION  | 1.0396  | 0.0000  | 0.1081 | 1.0000 | 1.07  |
| Losses = YES    | FES   | 6.1778  | 0.0000  | 0.2582 | 1.0000 | 1.09  |

The OSL illustrates this trend with an increase of 24% in PSH storage usage midday, allowing a system operator to dissipate stored energy at the evening peaks. For PSH storage network congestion increased the OSL fifteen-fold system-wide from the base case. However, considering losses yielded no significant changes.





## Storage Investment Results



### Impact of Renewable Penetration on Investment per Technology [MWh]

| Casa Study       | Tech Wind production |        |        |       |       |       |       |
|------------------|----------------------|--------|--------|-------|-------|-------|-------|
| Case Study       | Tech                 | x 0.25 | x 0.50 | x 1.0 | x 2.0 | x 2.5 | x 3.0 |
|                  | PSH                  | 0      | 0      | 0     | 0     | 9     | 206   |
| Congestion = NO  | CAES                 | 0      | 0      | 0     | 0     | 103   | 535   |
| Losses = NO      | LION                 | 0      | 0      | 0     | 0     | 0     | 55    |
|                  | FES                  | 200    | 200    | 211   | 237   | 298   | 0     |
|                  | PSH                  | 0      | 0      | 0     | 0     | 19    | 211   |
| Congestion = NO  | CAES                 | 0      | 1      | 0     | 0     | 123   | 538   |
| Losses = YES     | LION                 | 0      | 0      | 0     | 0     | 0     | 57    |
|                  | FES                  | 204    | 204    | 217   | 257   | 312   | 0     |
| 1                | PSH                  | 0      | 0      | 0     | 0     | 49    | 398   |
| Congestion = YES | CAES                 | 1      | 1      | 0     | 0     | 209   | 965   |
| Losses = NO      | LION                 | 0      | 0      | 0     | 0     | 14    | 116   |
|                  | FES                  | 188    | 266    | 212   | 363   | 309   | 16    |
|                  | PSH                  | 0      | 0      | 0     | 0     | 53    | 373   |
| Congestion = YES | CAES                 | 0      | 1      | 0     | 0     | 204   | 818   |
| Losses = YES     | LION                 | 0      | 0      | 0     | 0     | 13    | 117   |
|                  | FES                  | 184    | 262    | 221   | 361   | 326   | 17    |

- For the cases at or below standard wind production, FES was the only storage technology invested in. This implies that the need for FES capacity may primarily be to provide general load balance as opposed to just dealing with fluctuations from volume of wind generation.
- However, when wind production rose there grew a need for largescale energy reservoirs instead of fast energy storage technology such as FES.

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#### FES investment per node [MWh]

| Congestion = NO & Losses = NO                            |                            |                             |                                     |                                  |                            |                            |                           |                                |                         |                        |                       |                            |                            | Co                          | nges                       | tion                               | = NO                          | ) & L                           | osse                  | s = Y   | ES                       |                          |                             |                            |                            |                       |                           |                          |
|--|----------------------------|-----------------------------|-------------------------------------|----------------------------------|----------------------------|----------------------------|---------------------------|--------------------------------|-------------------------|------------------------|-----------------------|----------------------------|----------------------------|-----------------------------|----------------------------|------------------------------------|-------------------------------|---------------------------------|-----------------------|---|--------------------------|--------------------------|-----------------------------|----------------------------|----------------------------|-----------------------|---------------------------|--------------------------|
| x 3.00   | 0                          | 0                           | 0                                   | 0                                | 0                          | 0                          | 0                         | 0                              | 0                       | 0                      | 0                     | 0                          | 0                          | 0                           | 0                          | 0                                  | 0                             | 0                               | 0                     | 0   | 0                        | 0                        | 0                           | 0                          | 0                          | 0                     | 0                         | 0                        |
| x 2.50   | 21                         | 21                          | 21                                  | 21                               | 21                         | 21                         | 21                        | 21                             | 21                      | 21                     | 21                    | 21                         | 21                         | 21                          | 30                         | 18                                 | 49                            | 30                              | 13                    | 42  | 19                       | 19                       | 19                          | 10                         | 6                          | 15                    | 26                        | 16                       |
| x 2.00   | 17                         | 17                          | 17                                  | 17                               | 17                         | 17                         | 17                        | 17                             | 17                      | 17                     | 17                    | 17                         | 17                         | 17                          | 13                         | 20                                 | 39                            | 26                              | 9                     | 37  | 16                       | 16                       | 16                          | 8                          | 5                          | 14                    | 23                        | 16                       |
| x 1.00   | 15                         | 15                          | 15                                  | 15                               | 15                         | 15                         | 15                        | 15                             | 15                      | 15                     | 15                    | 15                         | 15                         | 15                          | 10                         | 12                                 | 26                            | 25                              | 3                     | 29  | 14                       | 14                       | 14                          | 9                          | 5                          | 12                    | 23                        | 21                       |
| x 0.50   | 14                         | 14                          | 14                                  | 14                               | 14                         | 14                         | 14                        | 14                             | 14                      | 14                     | 14                    | 14                         | 14                         | 14                          | 9                          | 11                                 | 19                            | 26                              | 2                     | 20  | 16                       | 16                       | 13                          | 10                         | 4                          | 11                    | 23                        | 24                       |
| x 0.25   | 14                         | 14                          | 14                                  | 14                               | 14                         | 14                         | 14                        | 14                             | 14                      | 14                     | 14                    | 14                         | 14                         | 14                          | 9                          | 11                                 | 18                            | 23                              | 4                     | 15  | 17                       | 17                       | 14                          | 11                         | 4                          | 12                    | 23                        | 26                       |
|  |                            |                             |                                     | Co                               | nges                       | tion                       | = YE                      | 5&1                            | Losse                   | es = N                 | 0                     |                            | 1                          |                             |                            |                                    |                               | Co                              | nges                  | tion =  | = YES                    | 5 & I                    | osse                        | s = Y                      | ES                         |                       |                           |                          |
|  | -                          | _                           |                                     |                                  | 0                          | 0                          | 0                         | 0                              | Ο                       | Δ                      | 0                     | 0                          | 0                          | 0                           | 0                          | 0                                  | 12                            | 1                               | 0                     | 0   | 0                        | 0                        | -                           |                            | 0                          | 0                     | 0                         | 0                        |
| x 3.00   | 0                          | 0                           | 13                                  | 0                                | 0                          | 0                          | 0                         | 0                              | 0                       | 0                      | 0                     | 0                          | 0                          | 0                           | 0                          | 0                                  | 15                            | 1                               | 0                     | 0   | 0                        | 0                        | 0                           | 0                          | 0                          | 0                     | 0                         | 0                        |
| x 3.00<br>x 2.50   | 0                          | 0                           | 13<br>189                           | 0<br>17                          | 5                          | 7                          | 14                        | 14                             | 12                      | 11                     | 9                     | 8                          | 8                          | 0<br>10                     | 5                          | 5                                  | 198                           | 1                               | 6                     | 30  | 10                       | 0<br>10                  | 0<br>10                     | 0<br>5                     | 3                          | 8                     | 12                        | 9                        |
| x 3.00<br>x 2.50<br>x 2.00                               | 0<br>2<br>4                | 0<br>2<br>25                | 13<br>189<br>281                    | 0<br>17<br>10                    | 0<br>5<br>1                | 7<br>2                     | 14<br>7                   | 14<br>7                        | 12<br>6                 | 11<br>5                | 9<br>4                | 8<br>2                     | 8<br>3                     | 0<br>10<br>4                | 5<br>1                     | 5<br>24                            | 198<br>275                    | 1<br>15<br>6                    | 6<br>1                | 30<br>15  | 10<br>6                  | 0<br>10<br>6             | 0<br>10<br>6                | 0<br>5<br>3                | 0<br>3<br>1                | 8<br>4                | 12<br>6                   | 9<br>6                   |
| x 3.00<br>x 2.50<br>x 2.00<br>x 1.00                     | 0<br>2<br>4<br>0           | 0<br>2<br>25<br>4           | 13<br>189<br>281<br>137             | 0<br>17<br>10<br>34              | 0<br>5<br>1<br>0           | 0<br>7<br>2<br>0           | 14<br>7<br>14             | 0<br>14<br>7<br>14             | 0<br>12<br>6<br>6       | 11<br>5<br>2           | 9<br>4<br>0           | 8<br>2<br>0                | 8<br>3<br>0                | 0<br>10<br>4<br>1           | 0<br>5<br>1<br>0           | 5<br>24<br>3                       | 198<br>275<br>135             | 1<br>15<br>6<br>36              | 6<br>1<br>0           | 0<br>30<br>15<br>3  | 0<br>10<br>6<br>6        | 0<br>10<br>6<br>6        | 0<br>10<br>6<br>1           | 0<br>5<br>3<br>2           | 0<br>3<br>1<br>0           | 8<br>4<br>6           | 12<br>6<br>12             | 9<br>6<br>10             |
| x 3.00<br>x 2.50<br>x 2.00<br>x 1.00<br>x 0.50           | 0<br>2<br>4<br>0<br>0      | 0<br>2<br>25<br>4<br>1      | 13<br>189<br>281<br>137<br>66       | 0<br>17<br>10<br>34<br>116       | 0<br>5<br>1<br>0<br>0      | 0<br>7<br>2<br>0<br>0      | 14<br>7<br>14<br>34       | 0<br>14<br>7<br>14<br>34       | 12<br>6<br>6<br>12      | 11<br>5<br>2<br>3      | 9<br>4<br>0<br>0      | 0<br>8<br>2<br>0<br>0      | 0<br>8<br>3<br>0<br>0      | 0<br>10<br>4<br>1<br>0      | 0<br>5<br>1<br>0<br>0      | 0       5       24       3       1 | 198<br>275<br>135<br>66       | 1<br>15<br>6<br>36<br>117       | 6<br>1<br>0<br>0      | 0<br>30<br>15<br>3<br>5   | 0<br>10<br>6<br>20       | 0<br>10<br>6<br>20       | 0<br>10<br>6<br>1<br>0      | 0<br>5<br>3<br>2<br>2      | 0<br>3<br>1<br>0<br>1      | 8<br>4<br>6<br>5      | 12<br>6<br>12<br>13       | 9<br>6<br>10<br>13       |
| x 3.00<br>x 2.50<br>x 2.00<br>x 1.00<br>x 0.50<br>x 0.25 | 0<br>2<br>4<br>0<br>0<br>0 | 0<br>2<br>25<br>4<br>1<br>1 | 13<br>189<br>281<br>137<br>66<br>50 | 0<br>17<br>10<br>34<br>116<br>81 | 0<br>5<br>1<br>0<br>0<br>0 | 0<br>7<br>2<br>0<br>0<br>0 | 14<br>7<br>14<br>34<br>24 | 0<br>14<br>7<br>14<br>34<br>24 | 12<br>6<br>6<br>12<br>6 | 11<br>5<br>2<br>3<br>1 | 9<br>4<br>0<br>0<br>0 | 0<br>8<br>2<br>0<br>0<br>0 | 0<br>8<br>3<br>0<br>0<br>0 | 0<br>10<br>4<br>1<br>0<br>0 | 0<br>5<br>1<br>0<br>0<br>0 | 0<br>5<br>24<br>3<br>1<br>1        | 198<br>275<br>135<br>66<br>50 | 1<br>15<br>6<br>36<br>117<br>81 | 0<br>6<br>1<br>0<br>0 | 0           30           15           3           5           1 | 0<br>10<br>6<br>20<br>10 | 0<br>10<br>6<br>20<br>10 | 0<br>10<br>6<br>1<br>0<br>0 | 0<br>5<br>3<br>2<br>2<br>1 | 0<br>3<br>1<br>0<br>1<br>0 | 8<br>4<br>6<br>5<br>5 | 12<br>6<br>12<br>13<br>12 | 9<br>6<br>10<br>13<br>13 |

- The transmission losses help to distinguish among the nodes for investment decisions in energy storage.
- However, if the network is congested then the investment decision are mainly driven by the network constraints. In this case, the network losses help to distinguish among the areas of the network that are not congested.

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### Conclusions and Future Research

#### Summary...



In an area with no congestion problems, losses are important to distinguish among the nodes in order to allocate ESS



Congestion is more relevant than losses and drives the allocation and investment decisions



Level of renewable penetration alters the optimal ESS technology investment decisions

#### Future work...



Use a more detailed model, such as Second Order Cone Programming (SOCP), in order to consider reactive and active power.

Stochastic model for uncertainty representation of multiple renewable profiles as scenarios in the future operation.





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